

Flexible Organic Electronics for Use in Neural Sensing

Hank Bink*, Yuming Lai*, Sangameshwar R. Saudari, Brian Helfer, Jonathan Viventi, Jan Van der Spiegel, *Fellow, IEEE*, Brian Litt, *Senior Member, IEEE*, Cherie Kagan

Abstract— Recent research in brain-machine interfaces and devices to treat neurological disease indicate that important network activity exists at temporal and spatial scales beyond the resolution of existing implantable devices. High density, active electrode arrays hold great promise in enabling high-resolution interface with the brain to access and influence this network activity. Integrating flexible electronic devices directly at the neural interface can enable thousands of multiplexed electrodes to be connected using many fewer wires. Active electrode arrays have been demonstrated using flexible, inorganic silicon transistors. However, these approaches may be limited in their ability to be cost-effectively scaled to large array sizes (8×8 cm). Here we show amplifiers built using flexible organic transistors with sufficient performance for neural signal recording. We also demonstrate a pathway for a fully integrated, amplified and multiplexed electrode array built from these devices.

I. INTRODUCTION

Electrocorticography (ECoG), the process of recording brain activity through electrodes placed directly on the cortical surface, is a common technique in the assessment and treatment of neurological disorders, such as epilepsy. ECoG offers a higher spatial and temporal resolution interface with the brain than extracranial EEG, since the electrodes are smaller and located at a much closer distance to the brain. Penetrating microelectrodes, such as the Utah array [1], can measure neural activity at a higher spatial resolution, including from single neurons, but are constrained to interface with small regions of the cortex. Further, the long-term feasibility of this interface is often limited to only

6-12 months [2], either due to tissue damage caused by the inability of the rigid penetrating electrodes to flex and move as the brain swells and contracts [3] or by damage caused from hemorrhage and inflammation from the initial insertion [4].

ECoG does not appear to suffer from this stability issue and has demonstrated consistent signal quality over extended periods of time with minimized irritation and injury to brain tissue [5], [6]. Further, ECoG and higher resolution micro-ECoG (μ ECoG) recordings from flexible arrays of non-penetrating electrodes may offer comparable information content to the neural signals recorded from penetrating electrodes in some applications, such as BMI [7]-[9], decoding motor control signals [10] and decoding spoken words [11]. High resolution neural interface is also important to understanding pathologic brain signals [12].

In addition to high spatial resolution, developing electrode arrays with a high degree of conformality is also important. Highly flexible arrays of electrodes have the ability to conform to the uneven patterns of sulci and gyri on the surface of the brain, resulting in higher signal to noise ratios in recordings and more electrodes in contact with the brain [13].

Current clinical ECoG arrays use metal electrodes that typically have a diameter of 3mm on a grid with 1cm center-to-center spacing [14]. Because of these dimensions, the arrays spatially undersample the electrical signals of the brain. μ ECoG electrode arrays have been developed that utilize flexible silicon electronics to create a conformal, dense (800 μ m spacing) electrode array capable of covering large areas (14.4mm x 12.8mm) of the brain [15]. These devices offer recordings with high spatial and temporal resolution and utilize on-chip multiplexing to reduce the number of wires coming off the grid. Constructing these silicon devices can be a difficult and expensive process. Alternatively, organic electronics may be able to be fabricated at lower cost than flexible silicon electronics on the same type of plastic substrates.

Organic materials are considered a promising candidate for flexible electronics due to the low temperatures required for fabrication. Through intensive research in the past decades, organic materials have been shown to exhibit carrier mobility comparable to or higher than amorphous silicon used in modern active-matrix liquid-crystal displays [16]. In addition, synthetic chemistry is able to tailor organic materials in a way that cannot be done with inorganics. The increased functionality of organic transistors can enable a broad array of biological signal monitoring applications.

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H. Bink (binkh@seas.upenn.edu) and J. Viventi are with the Bioengineering Department, University of Pennsylvania, Philadelphia, PA 19104 USA.

Y. Lai (yumingl@seas.upenn.edu) and J. Van der Spiegel are with the Electrical and Systems Engineering Department, University of Pennsylvania.

S.R. Saudari is with the Materials Science and Engineering Department, University of Pennsylvania

B. Helfer is with the Electrical and Computer Engineering Department, University of Connecticut, Storrs, CT 06269

C. Kagan (kagan@seas.upenn.edu) is with the Departments of Electrical and Systems Engineering, Materials Science and Engineering, and Chemistry, University of Pennsylvania.

B. Litt (littb@mail.med.upenn.edu) is with the Departments of Bioengineering and Neurology, University of Pennsylvania.

*H. Bink and Y. Lai contributed equally

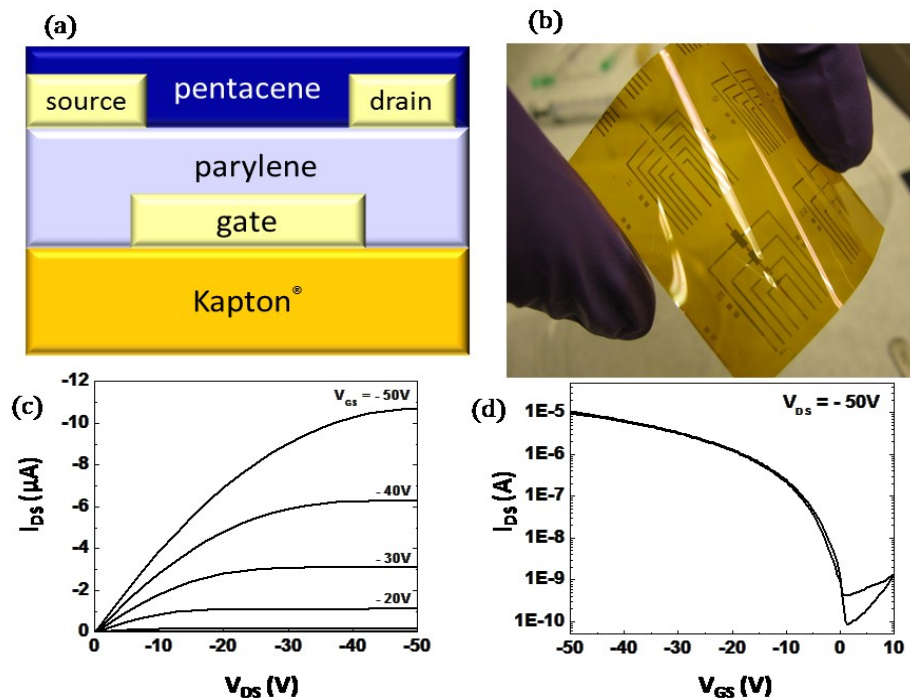


Fig. 1. (a) Schematic of the organic thin film transistor, a photographic example of which is seen in (b). (c) and (d) are the representative I_D - V_{DS} and I_D - V_{GS} properties of the devices, respectively. The channel width is $1500\mu\text{m}$ and length is $100\mu\text{m}$. These properties were measured in an inert nitrogen environment.

Pentacene, among the highest performance organic thin film semiconductor materials available, is insoluble in most organic solvents. A soluble pentacene precursor, developed by A. Afzali et al. [17], can be dissolved in a chlorinated solvent, such as chloroform, and subsequently thermally converted into pentacene. This production technique opens the door to large area fabrication of organic transistor circuits at low cost.

In this paper, we demonstrate solution processable organic thin film transistors that can be integrated directly into neural electrode arrays. We developed photolithographic methods to fabricate flexible organic thin film transistors. Combining these devices with custom circuits, we demonstrate common source and common drain amplifier topologies with performance sufficient for recording neural signals.

II. MATERIALS AND METHODS

Pentacene thin film transistors (TFTs) were fabricated in bottom-gate, bottom-contact configuration on a Kapton® substrate according to the method described in [18] and [19]. A schematic of the device is illustrated in Fig. 1(a). Gold gate and source/drain contacts were patterned by photolithography with a thickness of 20nm. A 500nm parylene-C dielectric layer was deposited through physical vapor deposition. The pentacene precursor was applied by spin-coating and then thermally converted to pentacene to form the bottom-gate, bottom-contact configuration TFT. Fig. 1(b) shows a photograph of the device electrodes before spin-coating the organic semiconductor.

Representative device characteristics measured under inert nitrogen environment are shown in Fig. 1(c) and Fig. 1(d).

Hole accumulation can be seen in the I_D - V_{DS} curve, characterized by linearity at low absolute drain-source biases and saturation at large negative biases. The saturation mobility is $0.123 \pm 0.038 \text{ cm}^2/(\text{V}\cdot\text{s})$, extracted from more than 50 transistors fabricated on different samples. The on/off current ratio is about 10^5 , as shown in I_D - V_{GS} curve (Fig. 1d).

The pentacene TFTs were tested in both common source and common drain amplifier configurations. A circuit consisting of all elements of the amplifying configurations except the transistor was created using a custom printed circuit board (PCB), which is shown in Fig. 2. In order to make the electrical connection between the pentacene TFTs on a flexible substrate and the PCB, the buried bottom gate had to be revealed. This was done by removing the pentacene over the electrode pads with chloroform. The parylene dielectric was then selectively etched with oxygen plasma, while keeping the active area protected. An additional small PCB with switches and finger-shaped beryllium copper contacts on the underside was designed to make mechanical contact with the flexible substrate of the transistor array. By clamping the small PCB onto the larger PCB with the flexible transistor array in between, the beryllium copper fingers are able to make solid mechanical contact with the electrodes of the transistor array, forming the electrical connection to the PCB. The pressure contact PCB is highlighted in yellow and enlarged in Fig 2. A short ribbon cable was used to connect the gate, source and drain of the organic transistor to their respective locations on the main PCB.

The circuit on the main PCB was designed to be used for either common source or common drain amplifying circuits. Since the source and drain of the organic transistors are

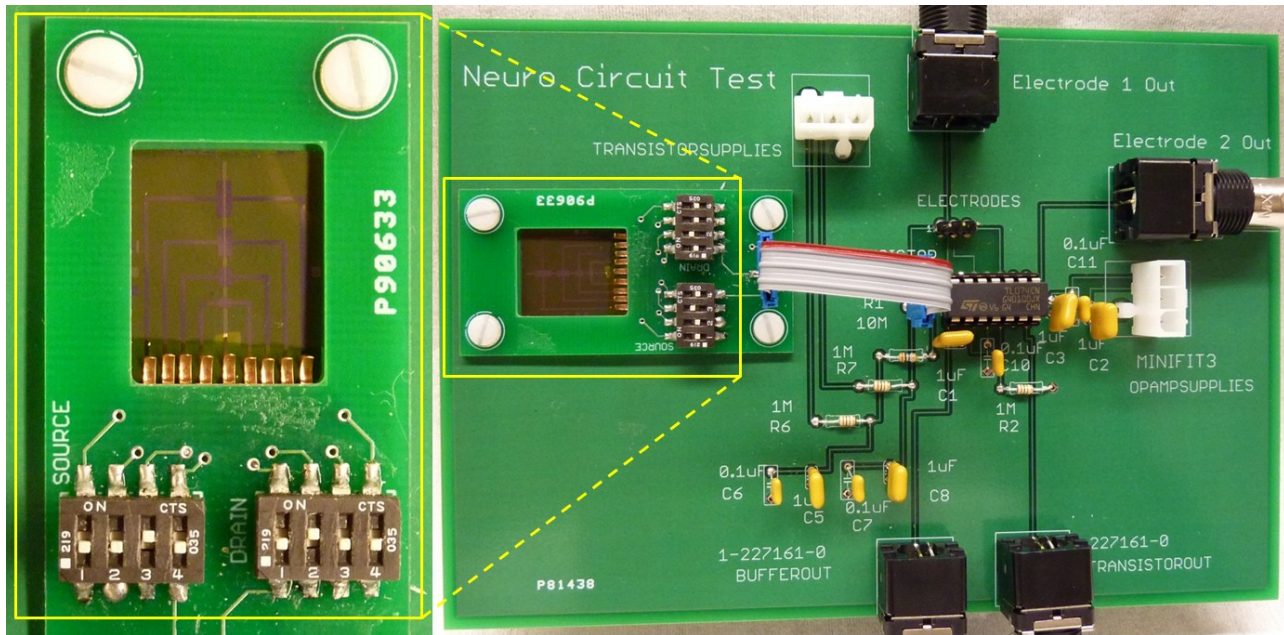


Fig. 2 The dual PCB board design. The large board contains all elements of the circuit excluding the transistor: the amplifying resistor, lowpass power supply filters, output buffer and highpass filter, and input/output components. The ribbon cable attaches the transistor to the rest of the circuit. The enlarged image on the left clearly shows the copper fingers used to make pressure contact with the organic TFT underneath.

interchangeable, switching between the two configurations was possible by changing power supply polarity. A $10\text{M}\Omega$ resistor was connected to the drain or source of the organic transistor depending on the desired circuit topology. This large resistance was used in order to yield higher gain. Power was supplied the organic transistor amplifier through 0.14 Hz low-pass filters in order to reduce noise coming from voltage supply electronics. The amplifier output was directly connected to a unity-gain buffer in order to reduce loading by subsequent measurement equipment.

III. RESULTS

The common source amplifier configuration was tested with multiple pentacene TFTs on the dual PCB setup. The source/drain transistor power supplies were kept at a difference of 50V . The maximum gain was 5.0dB for the highest performance device, while the average gain was 2.3dB . Fig. 3(a) shows a characteristic input/output voltage response for the best transistor with a $100\mu\text{m}$ channel. The source supply was $+28\text{V}$ and the drain supply was -22V . The input was a 1V_{pp} 10Hz sine wave. The output is inverted due to the common source topology.

The frequency response for the same organic transistor amplifier in the common source configuration is shown in Fig. 3(b). The -3dB cutoff was observed between 700 and 850Hz , depending on the transistor used. The square wave response rise and fall time of the amplifier was found to be 0.5ms each.

The common drain topology was tested by reversing the polarity of the TFT power supplies, effectively exchanging the source and drain. The maximum output of the device with a 1V_{pp} input was 0.65V_{pp} , or an attenuation of 3.7dB . A

frequency sweep revealed a -3dB bandwidth of 2.8kHz , much higher than the common source circuit, as expected.

IV. DISCUSSION AND CONCLUSIONS

The gain of the common source amplifier using pentacene TFTs (between 2.3 and 5dB) is promising for use in neural amplifiers. Current ECoG arrays use either passive electrodes or common drain amplifiers with unity gain. Integrating any level of gain directly at the electrode should improve the overall system performance. The attenuation seen in the organic transistor in common drain configuration, 3.7dB , would decrease the overall system performance, but would still be acceptable for many neural signal acquisition tasks.

The tradeoff for increased gain is decreased bandwidth: $\sim 800\text{Hz}$ for the common source configuration versus $\sim 2.8\text{kHz}$ for the common drain configuration. Given that the majority of clinically relevant, cortical surface brain activity occurs below 500Hz [20], a bandwidth of 800Hz would be sufficient for most applications. However, developing multiplexed electrode arrays may be difficult, given the low frequency response of the transistors.

One of the challenges faced while testing the amplifiers was the performance reduction of the pentacene TFTs in ambient atmosphere. Devices were initially characterized directly after fabrication, while still immersed in a pure nitrogen environment. The devices were subsequently retested after being exposed to open air. Carrier mobility, and likewise drain current, both continuously decreased as a result of exposure to moisture and oxygen. Several different encapsulating materials were applied to the TFTs in preliminary attempts to prevent this degradation. None of the materials so far investigated effectively protected the devices

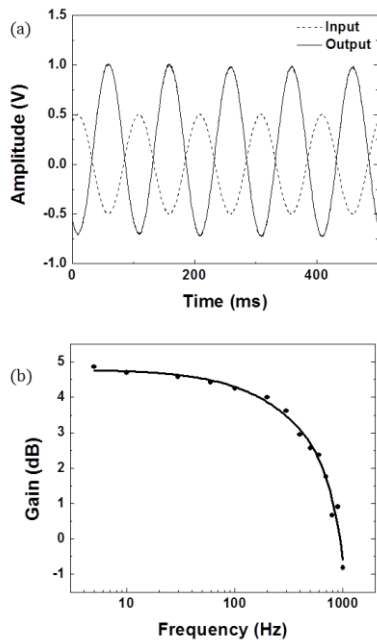


Fig. 3 Results from common source amplifier using pentacene TFT showing the (a) representative output versus input and (b) bode plot. Both results shown were taken from the same 100 μ m channel length device.

from reduction in their performance while exposed to air.

There are several items remaining to be addressed before organic transistors can be used to develop large arrays of multiplexed electrodes. First, the noise performance of the organic transistor amplifiers will be evaluated to insure sufficient signal to noise levels in the final system, while measuring neural signals of 1 mV amplitude or less. Initial noise measurements appear promising.

Second, the ability to pattern hundreds of organic transistors on a single flexible substrate will need to be developed. Prototypes of such devices have been fabricated, utilizing etching and deposition processes to create vertical integration access (VIA) holes to connect individual transistors using multiple metal layers.

Finally, a new encapsulation system will need to be developed to fully protect the transistors from exposure to air and biological fluids. New fabrication procedures and encapsulation materials are being evaluated for their long term reliability.

The devices described in this paper have been shown to work as amplifiers with adequate gain and bandwidth required for clinical and research neural sensor applications. While additional advancements are necessary, the potential advantages of organic μ ECoG electrode arrays motivate continued research to bring them to fruition.

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